

Derivation of a continuum description of sheared jammed soft suspensions from particle dynamics

Eric Bertin, Nicolas Cuny, Romain Mari

LIPhy, CNRS and Univ. Grenoble Alpes
Grenoble, France

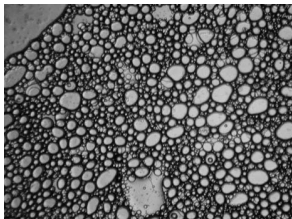
GdR IDE meeting
Grenoble, 29 November 2022



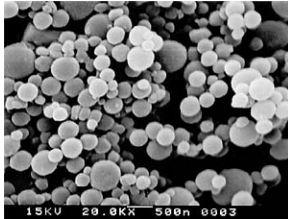
Soft jammed suspensions

Small soft particles packed in a fluid

Concentrated emulsion



Microgel suspensions



[Fréchet lab, UC Berkeley]

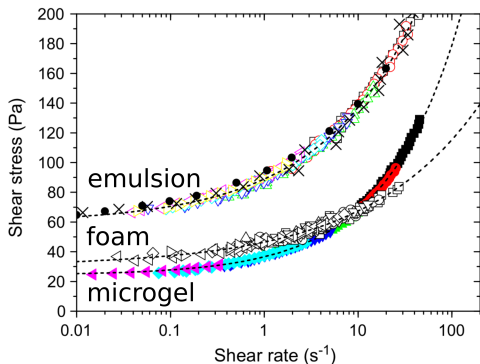
Rheology of yield stress fluids

Stationary flow curve

- Hershel-Bulkley behavior in simple shear (yield stress σ_y)

$$\sigma = \sigma_y + k\dot{\gamma}^n \quad (0 < n < 1)$$

- $n = 1$: limit case of a Bingham fluid



[Ovarlez et al.,
JNNFM 2013]

Rheological models

Phenomenological constitutive models

- Relate stress tensor Σ to strain tensor $\mathbf{E} = \frac{1}{2}(\nabla\mathbf{v} + \nabla\mathbf{v}^T)$
- *Viscoelastoplastic* models

$$\frac{\mathcal{D}\Sigma}{\mathcal{D}t} = \frac{2\eta}{\tau_{el}}\mathbf{E} + f(\Sigma), \quad f(\Sigma) \text{ to be determined}$$

- Von Mises yield criterion: plastic flow when $|\Sigma'| > \sigma_y$
(Σ' = deviatoric/traceless part of Σ)
- For a Bingham fluid [Saramito, JNNFM 2007]

$$f(\Sigma) = -\frac{1}{\tau_{el}} \max\left(0, \frac{|\Sigma'| - \sigma_y}{|\Sigma'|}\right) \Sigma$$

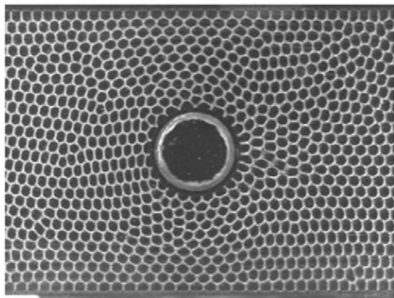
- Can be adapted to provide Hershel-Bulkley [Saramito, 2009]
- No microscopic guidance for $f(\Sigma)$, purely phenomenological

Rheological models

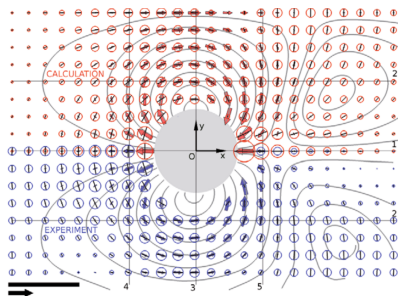
Experimental test of viscoelastoplastic models

$$\frac{D\Sigma}{Dt} = \frac{2\eta}{\tau_{el}} \mathbf{E} - \frac{1}{\tau_{el}} \max\left(0, \frac{|\Sigma'| - \sigma_y}{|\Sigma'|}\right) \Sigma$$

Foam flow around an obstacle under pressure gradient



[Cheddadi et al., EPJE 2011]



Top: theory, bottom: experiment

Open questions

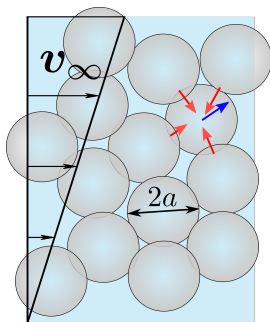
- Microscopic grounding?
- Can one *derive* a viscoelastoplastic constitutive law from a given microscopic dynamics of soft particles?

A minimal suspension model

- Overdamped soft disks, no hydrodynamic interactions
- Equation of motion of particle i (2D, athermal)

$$-\lambda(\mathbf{v}_i - \mathbf{v}_\infty(\mathbf{r}_i)) + \sum_{j \neq i} \mathbf{F}(\mathbf{r}_j - \mathbf{r}_i) = 0$$

System driven by flow field $\mathbf{v}_\infty(\mathbf{r})$, with uniform gradient $\nabla \mathbf{v}_\infty$



Probabilistic description

Exact evolution equation for the pair correlation function $g(\mathbf{r})$

$$\partial_t g(\mathbf{r}) + \nabla \cdot \mathbf{J}(\mathbf{r}) = 0$$

with probability flux

$$\mathbf{J}(\mathbf{r}) = \nabla v_\infty \cdot [\mathbf{r} \otimes g(\mathbf{r})] - \mathbf{F}(\mathbf{r})g(\mathbf{r}) - \rho \int \mathbf{r}' g_3(\mathbf{r}, \mathbf{r}') d\mathbf{r}'$$

Exact stress dynamics

- Microscopic definition of stress tensor

$$\Sigma = \frac{1}{V} \sum_{j \neq i} (\mathbf{r}_j - \mathbf{r}_i) \otimes \mathbf{F}(\mathbf{r}_j - \mathbf{r}_i) = \frac{\rho^2}{2} \int d\mathbf{r} \mathbf{r} \otimes \mathbf{F}(\mathbf{r}) g(\mathbf{r})$$

- Stress evolution: multiply by $\mathbf{r} \otimes \mathbf{F}(\mathbf{r})$ and integrate over \mathbf{r}

$$\partial_t \Sigma = \nabla v_\infty \cdot \Sigma + \Sigma \cdot \nabla v_\infty + \mathbf{S}_2[g(\mathbf{r})] + \mathbf{S}_3[g_3(\mathbf{r}, \mathbf{r}')]]$$

e.g., $\mathbf{S}_3 = -\frac{\rho^3}{2} \int [\mathbf{F}(\mathbf{r}') \otimes \mathbf{F}(\mathbf{r}) + \mathbf{r} \otimes \mathbf{F}(\mathbf{r}') \cdot (\nabla \mathbf{F}(\mathbf{r}))^T] g_3(\mathbf{r}, \mathbf{r}') d\mathbf{r} d\mathbf{r}'$

- Standard result for colloidal suspensions

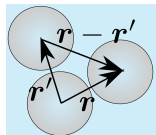
[Batchelor 70s; Russel 80s, 90s; Brady 90s; Morris 2010s,...]

- **Need to close stress dynamics**

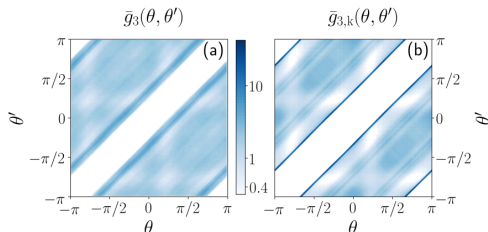
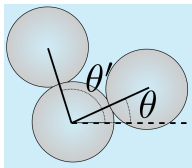
Microstructure closure

Approximate g_3 in terms of g

- Simplest assumption: Kirkwood closure
 $\bar{g}_3(\mathbf{r}, \mathbf{r}') \approx g(\mathbf{r})g(\mathbf{r}')g(\mathbf{r} - \mathbf{r}')$



- Numerical test in contact area (LAMMPS simulations, $\phi = 0.875$)

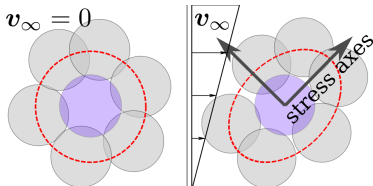


$$\bar{g}_3(\theta, \theta') = \int_{r, r' < 2a} r dr r' dr' g_3(\mathbf{r}, \mathbf{r}')$$

$$\bar{g}_{3,k}(\theta, \theta') = \int_{r, r' < 2a} r dr r' dr' g(\mathbf{r})g(\mathbf{r}')g(\mathbf{r} - \mathbf{r}')$$

Stress closure

Parametrize $g(\mathbf{r})$ with Σ'



Anisotropy expansion

$$\begin{aligned}g(\mathbf{r}) &= g_{\text{rest}} \left(\frac{|\mathbf{r}|}{1 - \alpha \mathbf{r} \cdot \Sigma' \cdot \mathbf{r} / |\mathbf{r}|^2} \right) \\ &= g_{\text{rest}}(|\mathbf{r}|) + \alpha g'_{\text{rest}}(|\mathbf{r}|) \frac{\mathbf{r} \cdot \Sigma' \cdot \mathbf{r}}{|\mathbf{r}|}\end{aligned}$$

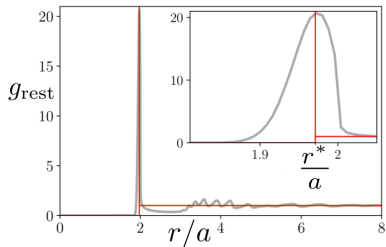
α is determined self-consistently

Stress closure

Minimal model for $g_{\text{rest}}(r)$

$$g_{\text{rest}}(r) \approx \frac{3}{\pi \rho r^*} \delta(r - r^*) + H(r - r^*)$$

- Dirac weight such that 6 nearest neighbors
[$H(r)$ Heaviside function]
- Nearest neighbor peak location $r^*(p)$, with pressure $p = -\frac{1}{2}\text{Tr}(\Sigma)$



Stress evolution equation

Lowest order approximation: $p = p(\phi)$

$$\partial_t \Sigma' = \kappa(\phi) \mathbf{E}_\infty + \mathbf{\Omega}_\infty \cdot \Sigma' - \Sigma' \cdot \mathbf{\Omega}_\infty + (\beta(\phi) - \xi(\phi) \Sigma' : \Sigma') \Sigma'$$

- Minimal form of the stress evolution equation

All coefficients $\kappa, \beta, \xi, \dots$ have **known** (but complicated) **expressions** in terms of packing fraction ϕ and microscopic parameters

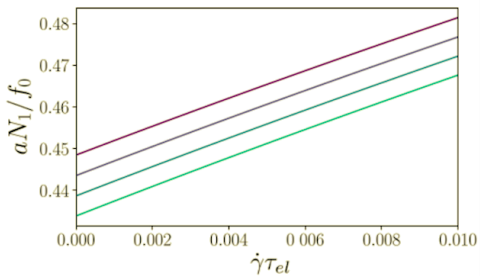
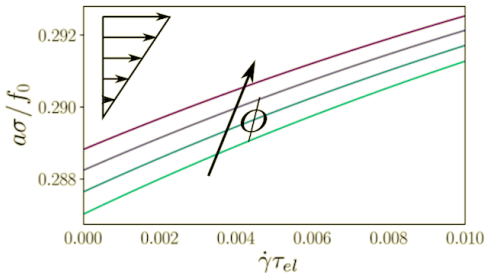
[Cuny, Mari, **EB**, PRL **127**, 218003 (2021); JSTAT 033206 (2022)]

Yield stress behavior

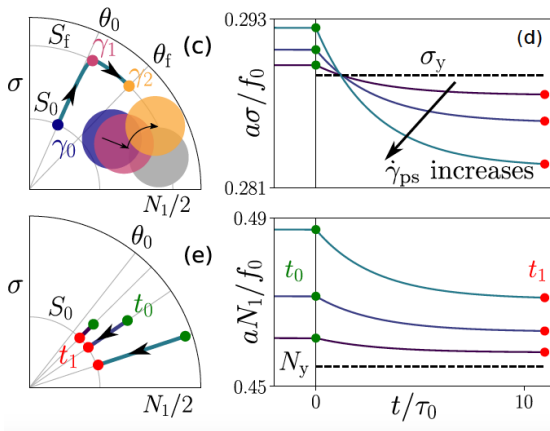
Bingham-like yield stress behavior for both shear stress σ and normal stress difference N_1

$$\Sigma' = \begin{pmatrix} N_1/2 & \sigma \\ \sigma & -N_1/2 \end{pmatrix}$$

[Cuny, Mari, **EB**, PRL (2021)]



Relaxation after a preshear



Polar representation (S, θ) : $N_1 = 2S \cos \theta$, $\sigma = S \sin \theta$
 S fast variable, θ slow variable for low shear rate $\dot{\gamma}$

[Cuny, Mari, **EB**, PRL (2021); Soft Matter (2022)]

Conclusion

- A constitutive model for jammed soft suspensions *derived from microscopics*
- **Reproduces important qualitative features:** yield stress, stress overshoot on step increase of shear rate, power-law decay in creep, etc.
[Cuny, Mari, **EB**, Soft Matter (2022)]
- **Outlook:** Try to improve closure approximations to get Hershel-Bulkley behavior and solid elastic branch